

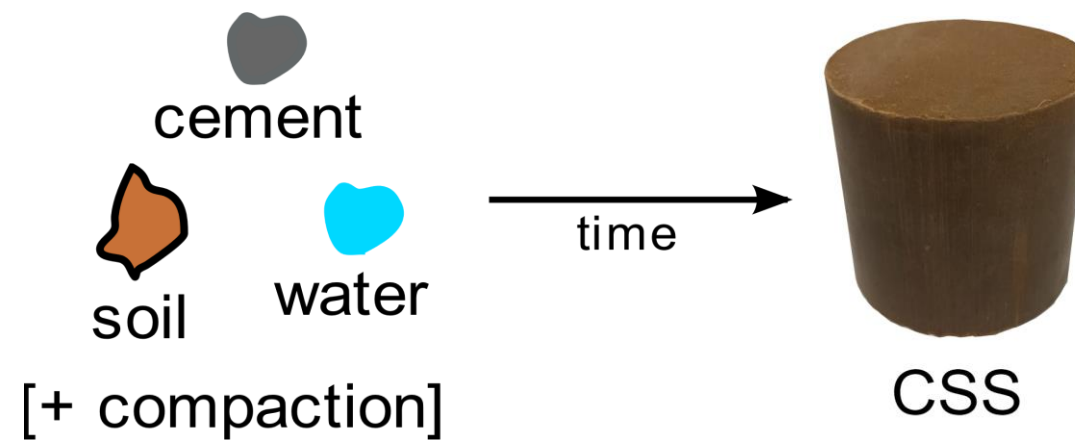
## CONTEXT

### Cemented-stabilized soils (CSS)<sup>[1]</sup>

in situ soil + hydraulic binder

- Reduction of environmental impact
- low-cost technique

Applications: embankments, foundations, pavement construction, retaining wall (RW)<sup>[2]</sup>



$$\text{Factor of Safety (FOS)} = \frac{\text{shear strength } \uparrow (?)}{\text{applied stress } \downarrow}$$

Failure criteria<sup>[2,3]</sup>  
Commonly not determined (empirical)  
Performance: tensile + compressive properties

CSS-RW analysis methods<sup>[2,4]</sup>  
Conventional vs Finite Element Modelling  
External vs internal stability

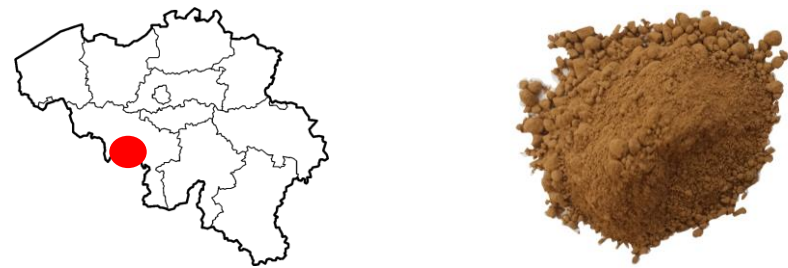
Empirical oversized design

**Objective:** Understand and verify consistency between mechanical characteristics of CSS and the stress states when employed as RW

## MATERIALS AND METHODS

### 1 Materials and treatment

"BC soil"



Soignies (Belgium)  
Covering soil - aggregate quarry

USCS %	LL = 30 %, IP = 13 %
Gravel 1	A = 0.29 (↓)
Sand 5	
Silt 70	
Clay 24	

[CL]

Standard proctor [3% cement content, CC]  
Optimum Moisture Content (OMC)  
Maximum Dry Density (MDD)

Binder [FR]  
Cement CEM II/A  
LL 42.5R CE CP 2

Mixture  
3% CC,  
96%MDD, OMC

### 2 Experiments

- (A) Indirect Tensile Strength, ITS (NF EN 13286-42)
- (B) Unconfined Compression Strength, UCS (NF EN 13286-41)
- (C) Direct Shear, DS (NF EN ISO 17892-10)

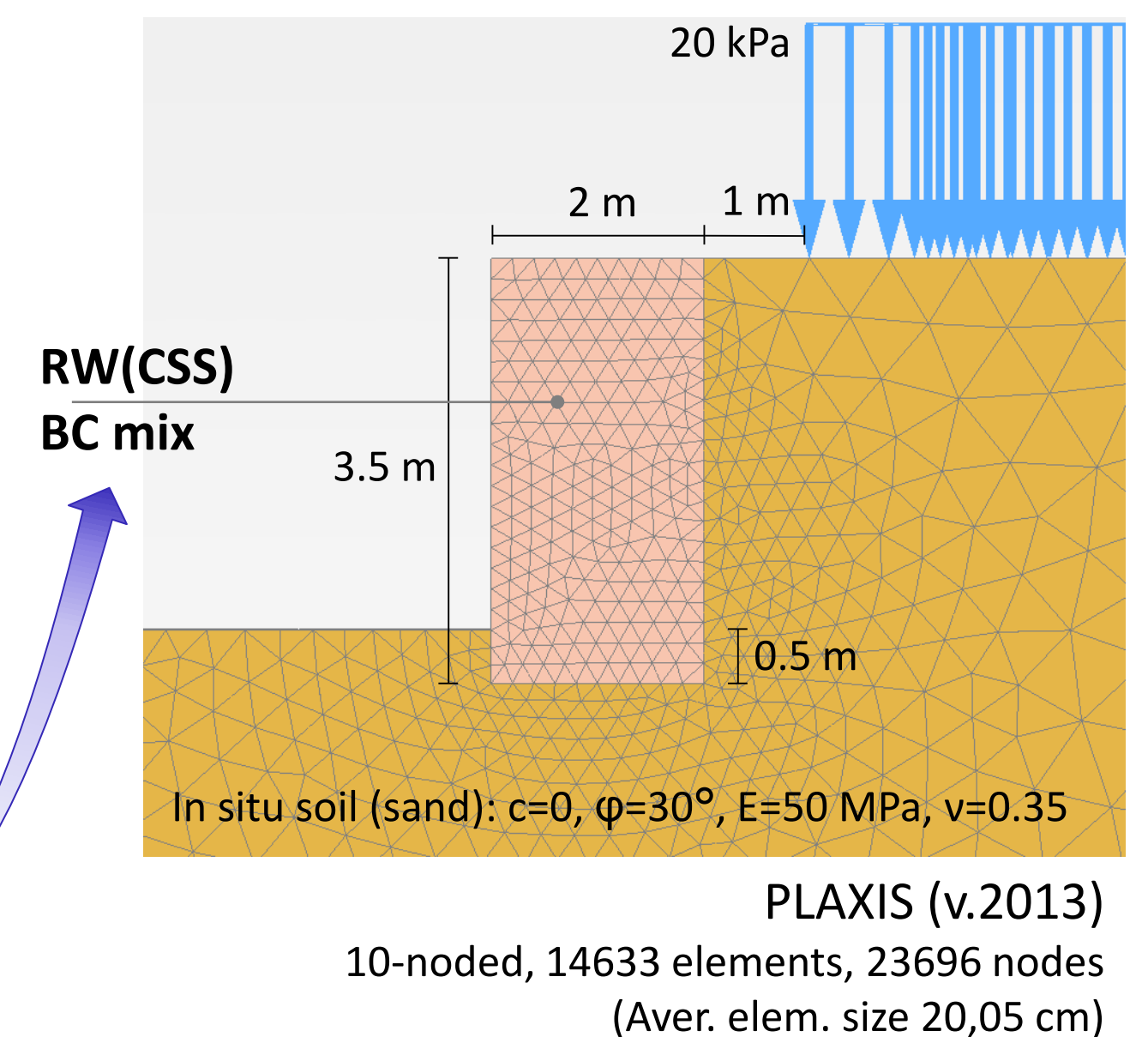


(D) Curing time (CT):  
7, 28, 90, 180, 360 days

ITS+UCS → Construction of failure criteria ← DS  
UCS → elastic parameters: elastic modulus (E), Poisson ratio (ν)

### 3 Finite Element Modelling, FEM

Elastic analysis, 2D



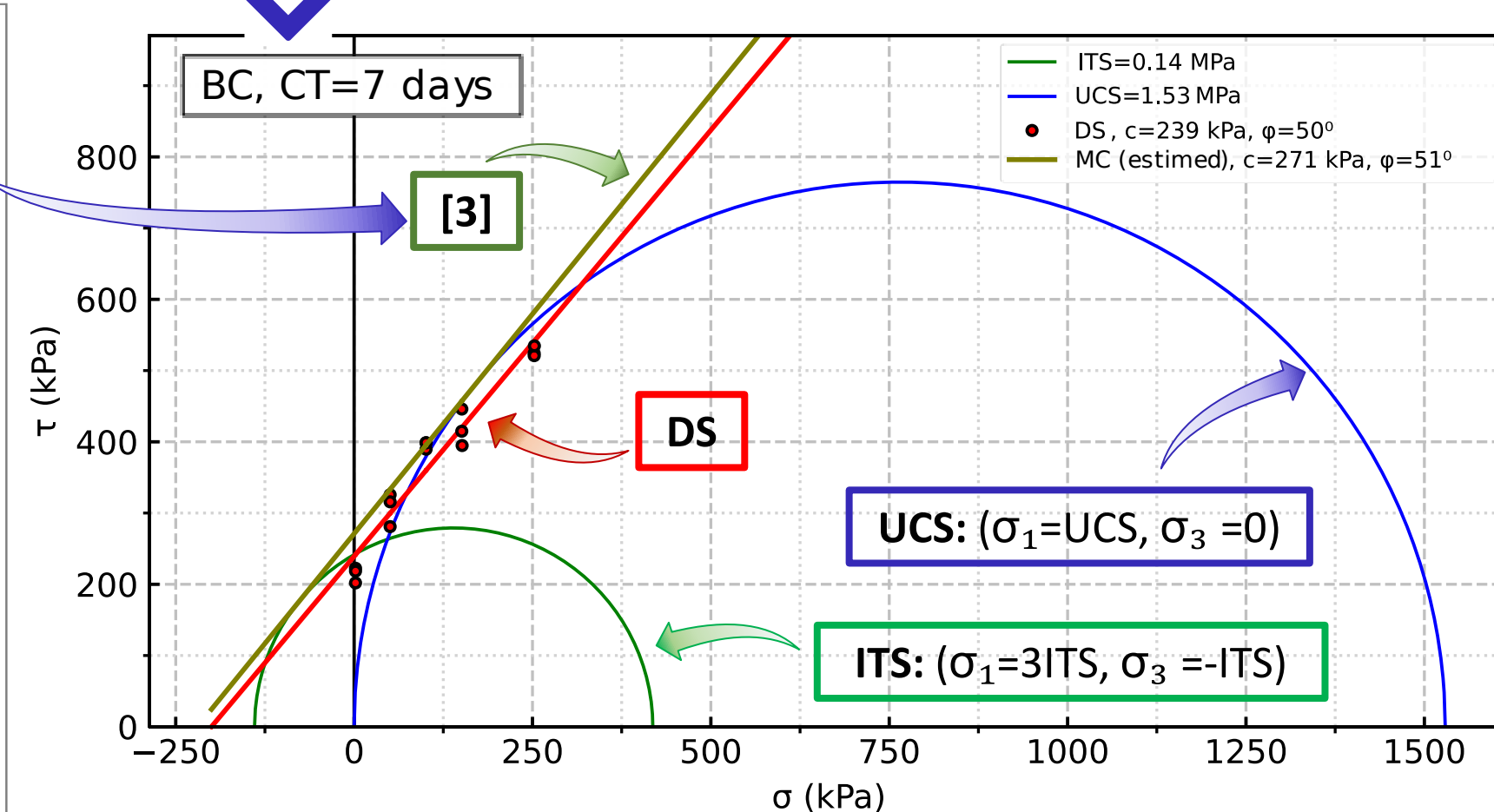
## RESULTS

### 1 Experimental results + assessment of MC failure envelope

CT (days)	7	28	90	180	360	
ITS (MPa)	0.14	0.15	0.18	0.23	0.22	
USC	UCS/E (MPa)	1.53 / 1459	1.65 / 1281	2.41 / 1672	1.77 / 969	2.11 / 1271
DS	c (MPa)	0.24 / 0.27	0.31 / 0.29	0.37 / 0.37	0.38 / 0.40	0.34 / 0.41
Experiment/[3]	φ' (°)	50.1 / 51.0	49.2 / 50.8	55.9 / 56.0	35.2 / 41.0	61.9 / 48.0

Simplified method for MC assessment<sup>[3]</sup>

If  
 $ITS = \lambda \times UCS$   
Then,  
 $\phi = f(\lambda)$   
and  
 $c = \begin{cases} f(\lambda, ITS) \\ \text{or} \\ f(\lambda, UCS) \end{cases}$



### 2 FEM (CT=7 days): c – φ reduction

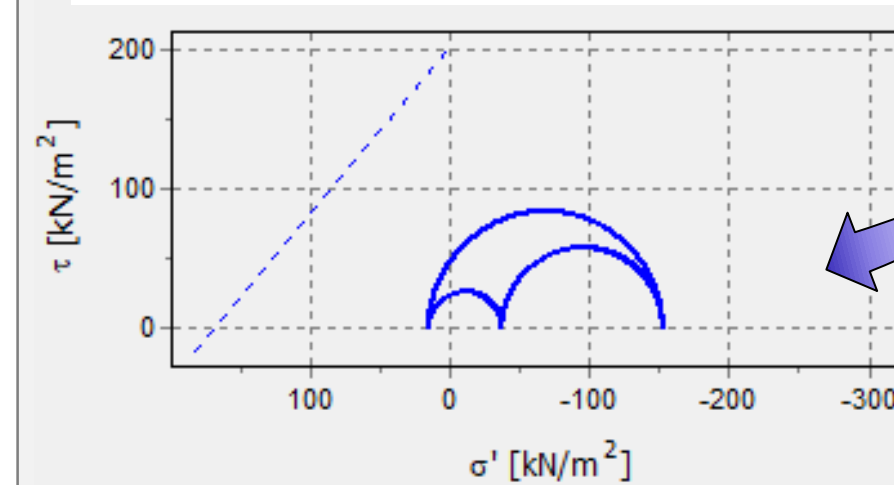
Relative shear stress,  $\tau_{rel}$

$$0.0 < \tau_{rel} = \frac{\tau_{max}}{\tau_{mob}} < 1.0$$

- Critical cohesion value (Ccrit.)
- Displac./stress pattern: external
- C = f(CC=3%, CT=7days) > Ccrit.

FOS

$$FOS = 1.2 = \frac{c}{c_{red}} = \frac{\tan \phi}{(\tan \phi)_{red}}$$



## CONCLUDING REMARKS

- Simplified method for MC assessment ✓
- $\phi = f(\lambda) \rightarrow$  independent of CC
- ITS and UCS interdepend parameters  $\rightarrow \lambda$
- C = f(UCS or ITS)  $\rightarrow$  validation of dosage techniques
- C = f(degree of cementation, CT)
- FEM – internal stability:  $\phi$ , cohesion  $\rightarrow$  Ccrit.
- CSS-RW: external failure for CT<7 days
- Failure pattern : overturning/bearing capacity (?)

## PERSPECTIVES

- Application of the simplified method on others CSS
- Sensibility study for durability evaluation
- Dosage optimization to obtain Ccrit.
- Conventional stability analysis for RW

## REFERENCES

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